

## INPUT/OUTPUT SIGNALS PRESERVER CIRCUIT OF AMPLIFICATION CIRCUITS

### Technical Field

5       The present invention relates to an input and output signal preservation circuit of an amplification circuit, and in particular to an input and output signal preservation circuit of an amplification circuit capable of preventing an attenuation of an input signal and an output signal of an amplification circuit in such a manner that an AC input signal is amplified using an amplification device  
10       such as a vacuum tube or a transistor in a preamplifier.

### Background Art

Figure 1 is a view of a small signal amplification circuit using a vacuum tube T1 as an amplification device wherein the vacuum tube T1 has been generally used for various audio systems. Here, the vacuum tube T1 can be substituted with a transistor.  
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As shown in Figure 1, in the vacuum tube T1 of the amplification circuit, a self-bias unit 10 is connected in the vacuum tube T1 wherein a bias resistor R1 is connected with a grid in parallel and has a resistor R2 and a condenser C1 that are connected with a cathode in parallel. The self-bias unit 10 amplifies  
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an AC input signal inputted into the grid and outputs to a plate.

The power unit 20 of the amplification circuit includes a smoothing unit 21 formed of a power transformer PT1, a rectifier T5, a resistor R4, and charging and discharging condensers C2 and C5 wherein the above elements 5 are coupled in the shape of  $\pi$ . The 220V input AC power is converted into a DC power (B+) by the power transformer PT1. The DC power (B+) rectified and smoothed through the rectifier T5 and the smoothing unit 21 is supplied to the plate through the load resistor R3 connected in parallel with the plate of the vacuum tube T1.

10 The coupling condenser C4 of the amplification circuit is connected with the plate output terminal of the vacuum tube T1 for thereby disconnecting the DC component of the amplification output signal Vo1.

In the thusly constituted amplification circuit, when the DC power (B+) is supplied to the plate signal that is the positive terminal of the vacuum tube T1, 15 the grid bias is generated at the resistor R2 of the self-bias unit 10 connected with the cathode that is the negative terminal of the vacuum tube T1 and the bias resistor R1 connected with the grid of the vacuum tube T1, respectively. Therefore, the vacuum tube T1 amplifies the AC input signal Vi1 inputted into the grid and outputs to the plate.

20 However, In the amplification circuit generally used in various audio

systems, the effective resistance values are changed due to the capacity between both terminals of the bias resistor R1, so that the AC input signal Vi1 could be leaked through the bias resistor R1. As a result, the grid input signal of the vacuum tube T1 that is the amplification device could be attenuated.

5        In the case that the resistance value of the bias resistor R1 is set larger than over a few values of MΩ in order to prevent the leakage of the AC input signal Vi1 through the bias resistor R1, the grid bias voltage Vg occurring by the bias resistor R1 is sharply increased. Therefore, the grid input current of the vacuum tube T1 is increased and is excessively oscillated, so that the vacuum  
10      tube T1 is broken.

Therefore, the conventional amplification circuit should adapt the bias resistor R1 having a resistance value lower enough for thereby preventing the damage of the vacuum tube T1 that has been used as an amplification device. In this case, it is impossible to prevent the leakage of the AC input signal Vi1.

15        In the above amplification circuit, since the effective resistance value is changed due to the capacity between both ends of the load resistor R3 of the output terminal, the amplification output signal Vo1 may be leaked through the resistor R3. As a result, the plate output signal of the vacuum tube T1 that is the amplification device could be attenuated.

20        In particular, in the above amplification circuit, since the capacity of the

coupling condenser C4 of the output terminal is set lower than the capacity of the charging and discharging condensers C2 and C5 included in the smoothing unit 21 of the power unit 20, the amplification output signal Vo1 is leaked through the charging and discharging condensers C2 and C5 of the smoothing unit 21. As a result, the plate output signal of the vacuum tube T1 that is the amplification device is attenuated.

In addition, In the above amplification circuit, the non-rectification AC component occurring due to the charging and discharging operations of the charging and discharging condensers C2 and C5 included in the smoothing unit 21 of the power unit 20 is mixed with the input and output signals Vi1 and Vo1, noises could be included in the input and output signals Vi1 and Vo1.

#### Disclosure of Invention

Accordingly, it is an object of the present invention to overcome the above-described problems encountered in the conventional art.

It is another object of the present invention to provide an input and output signal preservation circuit of an amplification circuit capable of increasing an input resistance value with respect to an AC input signal by connecting an input signal preservation electric device with an input terminal of an amplification circuit and increasing an output resistance value with respect to an

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amplification output signal by connecting an output signal preservation electric device with an output terminal of the amplification circuit, for thereby preventing an attenuation of an input signal and an output signal, respectively.

To achieve the above objects, in an amplification circuit using amplifying devices in a pre-amplifier in an audio system, there is provided an input and output signal preservation circuit of an amplification circuit, comprising an input signal preservation unit that is connected with an input terminal of an amplification device of an amplification circuit capable of amplifying an AC input signal using a certain amplification device and outputting the same and increases an input resistance value with respect to the input signal and prevents an attenuation of the input signal; and an output signal preservation unit that is connived with an output terminal of the amplification device and increases an output resistance value with respect to the amplification signal and prevents an attenuation of the amplification output signal for thereby compensating a voltage variation ratio with respect to the amplification output signal.

**Brief Description of Drawings**

The preferred embodiments of the present invention will be described with reference to the accompanying drawings.

20 Figure 1 is a view illustrating the construction of a conventional small

signal amplification circuit;

Figure 2A is a view illustrating the construction of a small signal amplification circuit adapting an input and output signal preservation circuit according to the present invention;

5       Figure 2B is a view of a resistance value variation characteristic measurement circuit and a characteristic table with respect to an AC input signal of a bias resistance;

Figure 2C is a view of an AC resistance value variation characteristic measurement circuit and a characteristic table with respect to an AC input 10 signal of a reactor;

Figure 2D is a view of an input resistance value variation characteristic measurement circuit and a characteristic table with respect to an AC input signal of an input signal preservation unit according to the present invention;

Figure 2E is a view of another input resistance value variation 15 characteristic measurement circuit and a characteristic table with respect to an AC input signal of an input signal preservation unit;

Figure 3 is a view illustrating the construction of a turntable phono-equalizer small signal amplification circuit adapting an input and output signal preservation circuit according an embodiment of the present invention;

20       Figure 4 is a view illustrating the construction of a tape equalizer small

signal amplification circuit adapting an input and output signal preservation circuit according to another embodiment of the present invention; and

Figure 5 is a view illustrating the construction of a power amplification circuit adapting an input and output signal preservation circuit according to  
5 another embodiment of the present invention.

#### **Best Mode for Carrying Out the Invention**

The first embodiment of the present invention will be described with reference to the accompanying drawings.

10 Figure 2A is a view of a state that an input and output signal preservation circuit according to the present invention is adapted to a small signal amplification circuit of Figure 1 adapting a vacuum tube T1 as an amplification device, wherein the vacuum tube has been used in various conventional audio systems as a pre-amplifier. Here, the vacuum tube T1 can  
15 be substituted with a transistor. The power unit 20 including the smoothing unit 21 of Figure 1 may be directly adapted. Therefore, the same reference numerals are given, and the descriptions of the same will be omitted.

As shown in Figure 2A, the input and output signal preservation circuit of the amplification circuit according to the present invention includes an input  
20 signal preservation unit 30 and an output signal preservation unit 40. The

Inventor of the present invention calls this circuit a 5A circuit or an Artist circuit and wants to indicate the same as AAAA.

The input signal preservation unit 30 includes a bias resistor R1 and a reactor L1 and is connected with an Input terminal of the vacuum tube T1 of the 5 amplification circuit for thereby preventing the attenuation of the input signal by increasing the input resistance value with respect to the AC input signal Vi1.

The inventor of the present invention calls the input signal preservation unit 30 formed of the bias resistor R1 and the reactor L1 as a 5A1 circuit.

The bias resistor R1 is connected with the grid input terminal of the 10 vacuum tube T1 in parallel.

The reactor L1 operates as an AC resistor with respect to the AC input signal Vi1 and is connected with the bias resistor R1 in series for thereby preventing a leakage of the AC input signal Vi1 by increasing the input resistance value.

15 The output signal preservation unit 40 includes an amplification signal preservation unit 41 formed of a load resistor R3 and a first reactor L2, and a voltage compensation unit 42 formed of a second reactor L3 and a condenser C3 and is connected with the output terminal of the vacuum tube T1 of the amplification circuit for thereby preventing an attenuation of the amplification 20 output signal Vo1 by increasing the output resistance value with respect to the

amplification output signal  $V_{o1}$  and compensating the voltage variation degree with respect to the amplification output signal  $V_{o1}$ .

The inventor of the present invention calls the output signal preservation unit 40 formed of the amplification signal preservation unit 41 and  
5 the voltage compensation unit 42 as a 5A2 circuit.

The load resistor  $R_3$  of the amplification signal preservation unit 41 is connected with the plate output terminal of the vacuum tube  $T_1$  in parallel.

The first reactor  $L_2$  of the amplification signal preservation unit 41 is connected with the load resistor  $R_3$  in series and operates as an AC resistor  
10 with respect to the amplification output signal  $V_{o1}$  for thereby preventing a leakage of the amplification output signal by increasing the output resistance value together with the load resistor  $R_3$ .

The second reactor  $L_3$  of the voltage compensation unit 42 is connected with a connection point of the load resistor  $R_3$  and the first reactor  $L_2$   
15 in parallel and operates as an AC resistor with respect to the amplification output signal  $V_{o1}$  for thereby preventing a leakage of the amplification output signal  $V_{o1}$  by increasing the output resistance value together with the load resistor  $R_3$ .

The condenser  $C_3$  of the voltage compensation unit 42 is connected  
20 with the second reactor  $L_3$  in series and compensates the voltage variation ratio

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of the amplification output signal.

The operation of the input and output signal preservation circuit according to the present invention adapted to the small signal amplification circuit used in various conventional audio systems as a pre-amplifier will be  
5 described with reference to the accompanying drawings.

The amplification circuit of Figure 2A operates identically to the amplification circuit of Figure 1. Actually, when a specific DC power (B+) is supplied to the plate side that is an anode of the vacuum terminal T1, a grid bias is formed at the resistor R2 of the self-bias unit 10 connected with the  
10 cathode that is a cathode of the vacuum tube T1 and a bias resistor R1 connected with a grid side of the vacuum tube T1 by the condenser C1, and the vacuum tube T1 amplifies the AC input signal Vi1 inputted into the grid and outputs to the plate.

At this time, the reactor L1 connected in series with the bias resistor R1  
15 of the input signal preservation unit 30 operates as an AC resistor with respect to the AC input signal Vi1 for thereby preventing a leakage of the AC input signal Vi1 by increasing the input resistance value together with the bias resistor R1.

Actually, the operation that the reactor L1 connected in series with the  
20 bias resistor R1 of the input signal preservation unit 30 increases the input

resistance value with respect to the AC input signal  $V_{I1}$  will be described with reference to Figures 2B through 2E.

Figure 2B is a view of a resistance variation characteristic measurement circuit and a characteristic table with respect to the AC input signal of the bias resistor  $R_1$ . As shown therein, the resistance values of the bias resistor  $R_1$  and the reference resistor  $R$  for measuring the resistance value variation of the bias resistor  $R_1$  are identically set to  $270\text{k}\Omega$ .

As shown in Figure 2B, when the AC input signal of which the amplitude is  $6\text{Vpp}$  and the current is  $I_1$  is inputted from the reference signal generator, 10 assuming that the frequency of the AC input signal is  $f=0\text{Hz}$ , the results are  $V_1+V=6\text{Vpp}$ , and  $I_1=6\text{V}/(R_1+R)=6\text{V}/(270\text{k}\Omega+270\text{k}\Omega) = 11.1\mu\text{A}$ .

However, the voltage measurement values of the bias resistor  $R_1$  measured by the oscilloscope and the reference resistor  $R$  have the amplitude variations of  $3.6\text{V} \sim 4.4\text{V}$  or  $2.6\text{V} \sim 1.6\text{V}$  with respect the frequency of 15  $20\text{Hz} \sim 20\text{kHz}$  of the AC input signal. Therefore, the bias resistor  $R_1$  has an effective resistance value changing with respect to the frequency change.

Therefore, as shown in Figure 2A, the bias resistor  $R_1$  of the grid input terminal of the vacuum tube  $T_1$  has an effective resistance value changing with respect to the frequency of the AC input signal  $V_{I1}$ . Therefore, it is needed to 20 use the minimum value DC bias for the reasons that the grid current may be

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sharply increased by the DC bias voltage, and the vacuum tube T1 may be damaged when the resistance value of the bias resistor R1 is set with over a few MΩ in order to preserve the grid input signal.

In addition, even when the resistance value of the bias resistor R1 is set  
5 with a minimum value in consideration with the change in the resistance value  
with respect to the AC input signal Vi1, the minimum set resistance value has a  
changing effective resistance value, and the changed value affects the DC grid  
current to be increased, so that the vacuum tube T1 may be damaged.  
Therefore, it is needed to set the resistance value to be lower than the above  
10 value. As the user of the bias resistor R1 having a low resistance value is used,  
the high frequency characteristic signal having a lower voltage of the AC input  
signal Vi1 or the ultra lower frequency and ultra harmonics disappear through  
the lower bias resistor R1 before they are inputted into the grids and are not  
inputted into the grids of the vacuum tube T1, so that the signal amplification  
15 does not occur in the high frequency characteristic signal or the ultra lower  
frequency and the ultra harmonics of the AC input signal Vi1.

Since the resistance value of the bias resistor R1 having a physical  
characteristic is changed by the frequency change of the AC input signal, as the  
frequency is increased based on  $f=1/T$  of the relationship between the  
20 frequency and the period, the time T is decreased, and the physical

characteristic is changed based on the change ( $\Delta T$ ) of the time. Therefore, the physical degree does not exist with respect to a very short time period, and the space is changed ( $\Delta S$ ). When the variation  $\Delta T$  of the time is extended to the time  $dT$ , and the variation  $\Delta S$  of the space is extended to  $dS$ , the variation  $dT$  of  
5 the time causes the variation  $dS$  of the space. The inventor of the present invention calls the above principle a time space deviation principle) in the descriptions of the present invention.

As shown in the characteristic table of Figure 2b, what the voltage of both ends of the measurement reference resistor R is changed is the same as  
10 what the voltage of both ends of the bias resistor R1 is changed based on the circuit characteristic. Therefore, there is shown that the resistance value of the bias resistor R1 of the measurement circuit using the same resistance value as the reference resistor R is changed. As shown in Figure 2B, there is shown a variation state of the effective resistance value of the bias resistor. The effects  
15 by the error of the measurement meter will be neglected.

Figure 2C is a view of an AC resistance value variation characteristic measurement circuit with respect to the AC input signal of the reactor. As shown therein, there are a 5H reactor L1, and a 250k $\Omega$  reference resistor R for the AC resistance value variation measurement of the reactor L1.

20 As shown in Figure 2C, when the AC input signal of which the

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amplitude is 6Vpp, and the current is I1 is inputted from the reference signal generator, the AC resistance of the reactor L1 is  $Z_L = \omega L = 2\pi fL = 2*3.14*5*f[\Omega]$  with respect to the frequency of the AC input signal. As the frequency of the AC input signal is increased, the AC resistance  $Z_L$  of the reactor L1 is flexibly  
5 increased.

Actually, the voltage measurement values of the reactor L1 and the reference resistor R measured by the oscilloscope has amplitude variations of 0V~2V or 6V~4V with respect to the frequency 20Hz~20kHz of the AC input signal. Therefore, it is known that the reactor L1 has an AC resistance value  
10 changing to  $2\pi fL$  with respect to the frequency variation.

For example, as shown in the characteristic table of Figure 2C, the AC resistance value is  $628\Omega$  at the low band of 20Hz, and this value could be considered to be approximate to  $0\Omega$ . There is not any voltage drop ( $V1=0V$ ) by the reactor L1, and the whole voltage is 6V at both end of the reference resistor  
15 R. In addition, since the voltage drop ( $V1$ ) of 2V corresponding to the AC resistor of occurs  $\omega L = 2\pi fL$  at both ends of the reactor L1 occurs at the high band of 20Hz, so that it is known that the voltage drop of 4V occurs at both ends of the reference resistor R.

Figure 2D is a view of an input resistance value variation characteristic  
20 measurement circuit and a characteristic table with respect to the AC Input

signal of the input signal preservation unit. As shown therein, there are provided a 270k $\Omega$  bias resistor R1, a 5H reactor L1, and a 270k $\Omega$  reference resistor R for the input resistance value variation measurement of the bias resistor R1 and the reactor L1.

5       As shown in Figure 2d, when the AC input signal of which the amplitude is 6Vpp and the current is I1 is inputted from the reference signal generator, the AC resistance Z<sub>L</sub> of the reactor L1 is  $Z_L = \omega L = 2\pi fL = 2*3.14*5*f[\Omega]$ . As the frequency of the AC input signal is increased, the AC resistance Z<sub>L</sub> of the reactor L1 is flexibly largely increased as shown in Figure 2C.

10      Figure 2E is a view of another input resistance value variation characteristic measurement circuit and a characteristic table with respect to an AC input signal of the input signal preservation unit. There are shown a 270 k $\Omega$  bias resistor R1 and a 5H reactor L1.

15      As shown in Figure 2E, when the AC input signal of which the amplitude is 6Vpp and the current is I1 is inputted from the reference signal generator, the AC resistance Z<sub>L</sub> of the reactor L1 is  $Z_L = \omega L = 2\pi fL = 2*3.14*5*f[\Omega]$ . As the frequency of the AC input signal is increased, the AC resistance Z<sub>L</sub> of the reactor L1 is flexibly largely increased as shown in Figure 2C.

20      As shown in Figures 2B through 2E, the effective resistance values are changed based on the voltage variation at both ends of the resistor in

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connection with the frequency change of the AC input signal of Figure 2B. The possible minimum resistance value is used like in the measurement circuit and a characteristic table of Figure 2E. In this embodiment, it is known that the voltage drop at both ends of the resistor is decreased based on the frequency  
5 increase of the AC input signal even when the grid bias current is minimized in the vacuum tube T1 of Figure 2A. Even when the frequency attenuation of the AC input signal is large at the bias resistor R1, it is possible to use the resistance value smaller than the minimum resistance value with respect to the bias resistor R1 in such a manner that the basic circuit is configured by  
10 connecting in series the reactor L1 to the bias resistor R1 and adding the input signal preservation unit 30 that the AC resistor ( $Z_L$ ) of the reactor L1 is added based on the increase of the frequency of the AC input signal.

In particular, in the basic principle of the input signal preservation unit 30, the grid input circuit of the vacuum tube T1 of Figure 2A is configured in  
15 such a manner that the audible frequency bands of 250Hz, 3kHz, 4kHz, 5kHz, 9kHz and harmonics that are too sensitive with respect to the high degree sound source protect the frequency characteristics of the sub-harmonic and ultra sub-harmonic and the ultra harmonic are protected. The series resonance is achieved at over 90kHz. There is provided a bias resistor R1 of which the AC  
20 resistor ( $Z_L$ ) of the reactor L1.

Meanwhile, when the vacuum tube T1 amplifies the AC input signal Vi1 inputted into the grid and outputs to the plate, the amplification output signal Vo1 disconnects the DC component by the coupling condenser C4.

At this time, the amplification signal preservation unit 41 formed the  
5 load resistor R3 and the first reactor L2 of the output signal preservation unit 40 operate in the same principle as the input signal preservation unit 30 and increases the output resistance value with respect to the amplification output signal Vo1 at the output terminal of the vacuum tube T1 of the amplification circuit for thereby preventing the attenuation of the amplification output signal  
10 Vo1.

The second reactor L3 of the output signal preservation unit 40 and the second reactor L3 of the voltage compensation unit 42 formed of the condenser C3 operate in the same principle as the reactor L1 of the input signal preservation unit 30 and the first reactor L2 of the output signal preservation unit 40. The output resistance value with respect to the amplification output signal Vo1 is increased at the output terminal of the vacuum tube T1 of the amplification circuit for thereby preventing the attenuation of the amplification output signal Vo1.  
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In particular, the condenser C3 of the voltage compensation unit 42  
20 compensates the voltage variation ratio with respect to the amplification output

signal Vo1 based on the charging and discharging operations of the charging and discharging condensers C2 and C5 included in the smoothing unit 21 of the power unit 20 for thereby stabilizing the bias voltage of the vacuum tube T1.

The second embodiment of the present invention will be described with  
5 reference to Figure 3.

Figure 3 is a view illustrating the construction that the input and output signal preservation circuit according to the present invention is adapted to the conventional phono equalizer small signal amplification circuit for the turntable in which two vacuum tubes T6 and T7 are adapted as a two-stage amplification 10 device. Here, the vacuum tubes T6 and T7 can be substituted with the transistors.

As shown in Figure 3, the input and output signal preservation circuit according to the present invention includes an input signal preservation unit 50 that is formed of a bias resistor R12 and a reactor L12 and is connected with an 15 input terminal of the first stage amplification vacuum tube T6, a voltage compensation unit 55 that is formed of a load resistor R17, a second reactor L13 and a condenser C18 and is connected with an output terminal of the first stage amplification vacuum tube T6, an input signal preservation unit 53 that is formed of a bias resistor R18 and a reactor L14 and is connected with an input 20 terminal of the second stage amplification vacuum tube T7, two load resistors

R20 and R21, a first reactor L16, a second reactor L17 and a condenser C21.

The output signal preservation unit 60 is connected with an outer terminal of the second stage amplification tube T7.

There is further provided an amplification signal preservation unit 54  
5 between the first stage amplification circuit and the second stage amplification circuit, namely between the voltage compensation unit 55 and the output signal preservation unit 60 wherein it is formed of the load resistor R19 and the first reactor L15 for compensating the voltage variation ratio with respect to the amplification output signal based on the amplification operation of the first stage  
10 amplification circuit and the second stage amplification circuit for thereby stabilizing the bias voltage of two vacuum tubes T6 and T7.

A self-bias resistor R14 is connected with a cathode of the first stage amplification vacuum tube T6. A time constant compensation unit 51 is formed of a series-connected resistor R13, a plurality of condensers C16 and C17 and  
15 resistors R15 and R16 for thereby compensating the time constant number of the AC input signal Vi3 and is connected with the self-bias resistor R14.

The power unit 20 including the smoothing unit 21 of Figures 1 and 2A is directly adapted. Therefore, the same reference numerals are adapted, and the descriptions of the same will be omitted.

20 The operation of the input and output signal preservation circuit

according to the present invention adapted to a conventional turntable phono-equalizer small signal amplification circuit will be described.

When a certain DC power (B+) of the power unit 20 is supplied to the plate side that is an anode terminal of the first stage amplification vacuum tube 5 T6, a grid bias of which a time constant is compensated by the time constant compensation unit 51 is formed at the bias resistor R12 connected with the grid side of the first stage amplification vacuum tube T6 by the self-bias resistor R14 connected with the cathode that is a cathode of the first stage amplification vacuum tube T6. Therefore, the first stage amplification vacuum tube T6 10 amplifies the AC input signal Vi3 inputted into the grid and outputs to the plate.

At this time, the reactor L12 connected in series with the bias resistor R12 of the input signal preservation unit 50 operates as an AC resistor with respect to the AC input signal Vi3 and includes the Input resistance value together with the bias resistor R12 for thereby preventing a leakage of the AC 15 Input signal Vi3.

The output signal amplified by the first stage amplification vacuum tube T6 disconnects the DC component by the coupling condenser C19 and is inputted into the grid of the second stage amplification vacuum tube T7.

At this time, the load resistor R17 and the second reactor L13 of the 20 voltage compensation unit 55 operate in the same principle as the input signal

- preservation unit 30 as shown in Figure 2A and increases the output resistance value with respect to the amplification output signal at the output terminal of the vacuum tube T6 of the first stage amplification circuit and prevents the attenuation of the amplification output signal. The condenser C18 of the voltage compensation unit 55 compensates the voltage variation ratio with respect to the amplification output signal based on the charging and discharging operations of the charging and discharging condensers C2 and C5 included in the smoothing unit 21 of the power unit 20 for thereby stabilizing the bias voltage of the first stage amplification vacuum tube T6.
- 10        The reactor L14 connected in series with the bias resistor R18 of the input signal preservation unit 53 of the second stage amplification vacuum tube T7 operates as the AC resistor with respect to the first amplified AC input signal and increases the input resistance value together with the bias resistor R18 for thereby preventing a leakage of the first stage amplified AC input signal.
- 15        As the first stage amplified AC input signal is inputted into the grid of the second stage amplification vacuum tube T7, the second stage amplification vacuum tube T7 second-stage amplifies the AC input signal and outputs to the plate, and the amplification output signal Vo3 disconnects the DC component based on the coupling condenser C20.
- 20        At this time, the amplification signal preservation unit 61 formed of two

load resistors R20 and R21 of the output signal preservation unit 60 and the first reactor L16 operates in the same principle as the input signal preservation unit 30 of Figure 2A and increases the output resistance value with respect to the amplification output signal Vo3 at the output terminal of the vacuum tube T7 of 5 the second stage amplification circuit for thereby preventing the attenuation of the amplification output signal Vo3.

In addition, the second reactor L17 of the output signal preservation unit 60 and the second reactor L17 of the voltage compensation unit 62 formed of the condenser C21 operate in the same principle as the reactor L1 of the input 10 signal preservation unit 30 of Figure 2A and the first reactor L2 of the output signal preservation unit 40 and increases the output resistance value with respect to the amplification signal Vo3 at the output terminal of the vacuum tube T7 of the second stage amplification circuit for thereby preventing the attenuation of the amplification output signal Vo3.

15 In particular, the condenser C21 of the voltage compensation unit 62 compensates the voltage variation ratio with respect to the amplification output signal Vo3 based on the charging and discharging operations of the charging and discharging condensers C2 and C5 included in the smoothing unit 21 of the power unit 20 for thereby stabilizing the bias voltage of the second stage 20 amplification vacuum tube T7.

The third embodiment of the present invention will be described with reference to the accompanying drawings.

Figure 4 is a view illustrating the construction that the input and output signal preservation circuit according to the present invention is adapted to the conventional tape equalizer small signal amplification circuit that uses two vacuum tubes T8 and T9 as the second stage amplification device.

Here, the vacuum tubes T7 and T8 can be substituted with the transistor.

In particular, Figure 4 is a circuit diagram illustrating the construction that the input and output signal preservation circuit according to the present invention is adapted to the conventional turntable phono-equalizer small signal amplification circuit using the second stage amplification device. There is a difference between the above embodiment and the second embodiment of Figure 3. Namely, in this embodiment of the present invention, the time constant compensation unit 71 connected in parallel with the self-bias resistor R24 connected with the cathode of the first stage amplification vacuum tube T8 is formed of a plurality of resistors R23 and R25 connected in parallel or series, and a plurality of condensers C22 and C26 for thereby compensating the time constant of the AC input signal Vi4.

The remaining constructions are the same as the second embodiment

of Figure 3, so that the construction and operation will be omitted.

The fourth embodiment of the present invention will be described with reference to Figure 5.

Figure 5 is a view illustrating a state that the input and output signal preservation circuit according to the present invention is adapted to the conventional power amplification circuit capable of outputting an amplification output signal  $V_{o2}$  through the output transformer OT1 using the three stage amplification device with respect to three vacuum tubes T2, T3 and T4 driven by the DC power supplied through the smoothing unit 121 in which the reactor L11 and the charging and discharging condensers C15 and C14 are coupled in a shape of  $\pi$ . Here, the vacuum tubes T2, T3 and T4 may be substituted with the transistor.

As shown in Figure 5, the first stage output signal preservation unit 140 includes an input signal preservation unit 130 formed of a bias resistor R5 and a reactor L4 and connected with an input terminal of the first stage amplification vacuum tube T2, an amplification signal preservation unit 141 formed of a load resistor R7 and a first reactor L6 and connected with an output terminal of the first stage amplification vacuum tube T2 and an input terminal of the second stage amplification vacuum tube T3, and a voltage compensation unit 135 formed of a second reactor L5 and a condenser C7 and connected in parallel

with the amplification signal preservation unit 141.

The second stage output signal preservation unit 150 includes an amplification signal preservation unit 152 formed of a load resistor R9 and a first reactor L8 and connected with an output terminal of the second stage 5 amplification vacuum tube T3 and an input terminal of the third stage amplification vacuum tube T4, and a voltage compensation unit 144 formed of a second reactor L7 and a condenser C9 and connected in parallel with the amplification signal preservation unit 150.

The voltage compensation unit 143 is formed of a second reactor L10 10 and a condenser C13 and is connected with a primary side of the output transformer OT1 connected with an output terminal of the third stage amplification vacuum tube T4.

The self-bias units 131, 141 and 151 are connected with the cathodes of the first, second and third amplification vacuum tubes T2, T3 and T4 and are 15 formed of the resistors and condensers R6, C6; R8, C8 and R10, C10, so that a grid bias is formed at the bias resistor R5 connected with a grid side of the first stage amplification vacuum tube T2.

The voltage compensation unit 155 is further connected at a connection point between the first stage amplification circuit and an output terminal of the 20 third stage amplification circuit, namely, at a rear end of the amplification signal

preservation unit 141 of the first stage output signal preservation unit 140 and at a connection point of the amplification signal preservation unit 151 of the second stage output signal preservation unit 150 for thereby compensating the voltage variation ratio with respect to the amplification output signal based on 5 the amplification operation of the first amplification circuit and the second amplification circuit for thereby stabilizing the bias voltages of two vacuum tubes T2 and T3.

The amplification signal preservation unit 125 is further connected between the second stage amplification circuit and an output terminal of the 10 third stage amplification circuit, namely, between the amplification signal preservation unit 151 of the second stage output signal preservation unit 150 and an output terminal of the third stage amplification vacuum tube T4 and is formed of a load resistor R11 and a first reactor L9 for thereby compensating the voltage variation ratio with respect to the amplification output signal based 15 on the amplification operation of the second stage amplification circuit and the third amplification circuit and stabilizing the bias voltages of two vacuum tubes T3 and T4.

The power unit 120 of the amplification circuit includes a smoothing unit 121 in which a power transformer PT1, a rectifier T5, a reactor L11, and 20 charging and discharging condensers C14 and C15 are coupled in a shape of  $\pi$ .

The common 220V input AC power is transformed into a specific DC power (B+) by the power transformer PT1 and supplies the DC power rectified and smoothed by the rectifier T5 and the smoothing unit 121.

The operation of the input and output signal preservation circuit  
5 according to the present invention adapted to the conventional three stage power amplification circuit will be described.

When the DC power of the power unit 120 is supplied to the plate that is the anode terminal of the first stage amplification vacuum tube T2, a grid bias is formed at the resistor R6 of the self-bias unit 131 and the bias resistor R5 connected with the grid of the first stage amplification vacuum tube T2, so that the first stage vacuum tube T2 amplifies the AC input signal Vi2 inputted into the grid and outputs to the plate.  
10

At this time, the reactor L4 connected in series with the bias resistor R5 of the input signal preservation unit 130 operates as the AC resistor with respect to the AC input signal Vi2 for thereby increasing the input resistance value together with the bias resistor R5 and preventing a leakage of the AC input signal Vi2.  
15

Thereafter, the output signal amplified by the first stage amplification vacuum tube T2 is inputted into the grid of the second stage amplification  
20 vacuum tube T3.

At this time, the load resistor R3 and the first reactor L6 of the amplification signal preservation unit 141 connected with an output terminal of the first stage amplification vacuum tube T2 operate in the same principle as the input signal preservation unit 30 of Figure 2A for thereby increasing an output resistance value with respect to the amplification output signal at the vacuum tube T2 of the first stage amplification circuit and the AC input signal of the second stage amplification vacuum tube T3 and preventing the attenuation of the amplification output signal (or AC input signal).

The second reactor L5 of the voltage compensation unit 135 connected with an output terminal of the vacuum tube T2 of the first stage amplification circuit operates in the same principle as the first reactor L1 of the input signal preservation unit 30 of Figure 2A and the first reactor L2 of the output signal preservation unit 40 and increases the output resistance value with respect to the amplification output signal (or AC input signal) at the output terminal of the vacuum tube T2 of the first state circuit for thereby preventing the attenuation of the amplification output signal (or AC input signal).

The condenser C7 of the voltage compensation unit 135 connected with an output terminal of the vacuum tube T2 of the first stage amplification circuit compensates the voltage variation ratio with respect to the amplification output signal (or AC input signal) based on the charging and discharging operation of

the charging and discharging condensers C15 and C14 contained in the smoothing unit 121 of the power unit 120 for thereby stabilizing the bias voltage of the first stage amplification vacuum tube T2.

Next, the second amplification vacuum tube T3 amplifies the AC input  
5 signal inputted into the grid after it is first-stage amplified by the first stage amplification vacuum tube T2 and outputs to the plate.

At this time, the load resistor R9 and the first reactor L8 of the amplification signal preservation unit 151 connected with an output terminal of the second stage amplification vacuum tube T3 operate in the same principle as  
10 the Input signal preservation unit 30 of Figure 2A and increases the output resistance value with respect to the amplification output signal at the output terminal of the vacuum tube T3 of the second stage amplification circuit, namely, the AC input signal of the third stage amplification vacuum tube T4 for thereby preventing the attenuation of the amplification output signal (or AC input signal).

15 The second reactor L7 of the voltage compensation unit 144 connected with an output terminal of the vacuum tube T3 of the second stage amplification circuit operates in the same principle as the reactor L1 of the input signal preservation unit 30 of Figure 2A and the first reactor L2 of the output signal preservation unit 40 and increases the output resistance value with respect to  
20 the amplification output signal (or AC input signal) at the output terminal of the

vacuum tube T3 of the second stage amplification circuit for thereby preventing the attenuation of the amplification output signal (or AC input signal).

The condenser C9 of the voltage compensation unit 144 connected with an output terminal of the vacuum tube T3 of the second stage amplification 5 circuit compensates the voltage variation ratio with respect to the amplification output signal (or AC input signal) based on the charging and discharging operations of the charging and discharging condensers C15 and C14 contained in the smoothing unit 121 of the power unit 120 for thereby stabilizing the bias voltage of the second stage amplification vacuum tube T3.

10 Finally, the third stage amplification vacuum tube T4 amplifies the AC input signal inputted into the grid after it is second-stage amplified by the second stage amplification vacuum tube T3 and outputs to the plate.

At this time, the second reactor L10 of the voltage compensation unit 143 connected with an output terminal of the third stage amplification vacuum 15 tube T4 operates in the same principle as the reactor L1 of the input signal preservation unit 30 of Figure 2A and the first reactor L2 of the output signal preservation unit 40 and increases the output resistance value with respect to the amplification output signal at the output terminal of the vacuum tube T4 of the third stage amplification circuit for thereby preventing the attenuation of the 20 amplification output signal.

The condenser C3 of the voltage compensation unit 143 connected with an output terminal of the vacuum tube T4 of the third stage amplification circuit compensates the voltage variation ratio with respect to the amplification signal based on the charging and discharging operations of the charging and 5 discharging condensers C15 and C14 contained in the smoothing unit 121 of the power unit 120 for thereby stabilizing the bias voltage of the third stage amplification vacuum tube T4.

#### Industrial Applicability

10 As described above, in the input and output preservation circuit of an amplification circuit according to the present invention, the input resistance values with respect to the AC input signal are increased by connecting the electric devices (for example, bias resistor and reactor) of the input signal preservation with an input terminal of the amplification circuit, and the output 15 resistance values are increased with respect to the amplification signal by connecting the electric devices of the output signal preservation with an output terminal of the amplification circuit for thereby preventing the attenuations of the input signal and the output signal. Therefore, in the present invention, the leakage problem of the AC input signal through the bias resistor connected with 20 an input terminal of the amplification circuit used in various audio systems is

overcome. The damaging problem of the amplification device occurring when the resistance value of the bias resistor is set larger than over a few MΩ in order to prevent the leakage of the AC input signal through the bias resistor can be prevented. The leakage problem of the amplification output signal through 5 the load resistor connected with an output terminal of the amplification circuit can be overcome. In addition, the leakage problem of the amplification output signal through the charging and discharging condenser included in the smoothing unit of the power unit of the amplification circuit can be prevented. The noise generation problem of the input and output signal occurring due to 10 the charging and discharging operations of the charging and discharging condensers can be overcome. Namely, all the conventional known problems can be overcome. The present invention is capable of achieving a super high end audio characteristic.

As the present invention may be embodied in several forms without 15 departing from the spirit or essential characteristics thereof, it should also be understood that the above-described examples are not limited by any of the details of the foregoing description, unless otherwise specified, but rather should be construed broadly within its spirit and scope as defined in the appended claims, and therefore all changes and modifications that fall within 20 the meets and bounds of the claims, or equivalences of such meets and bounds

are therefore intended to be embraced by the appended claims.